

# Modification of design in PL series vacuum pump to enhance performance of pump

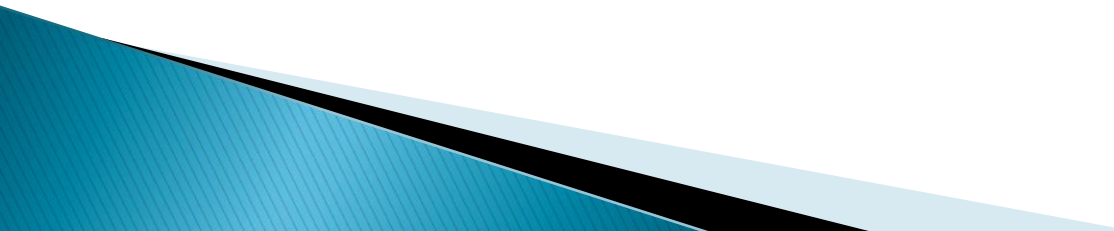


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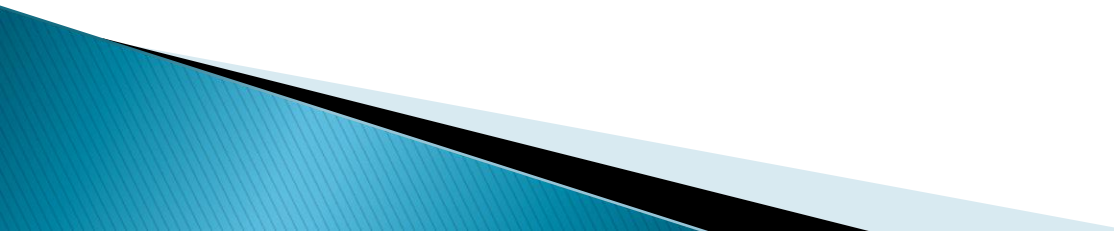
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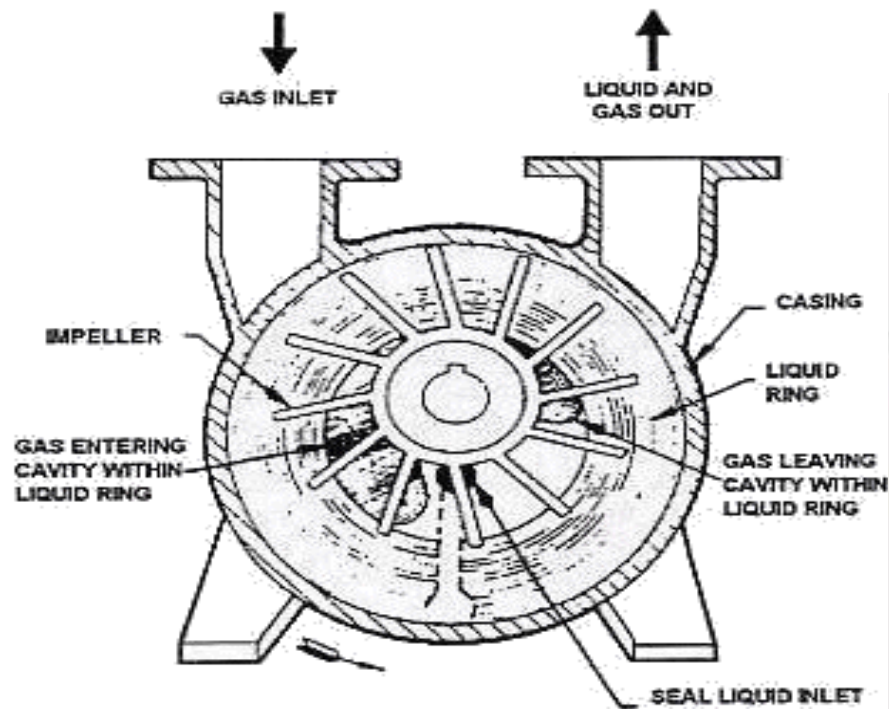
# Contents of Project

- ▶ Introduction
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  - ▶ Different parts of the pump
  - ▶ Calculation
  - ▶ Analysis of the impeller
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# Introduction

- ▶ A pressurized liquid vacuum pump is a rotating positive displacement pump. It is also known as liquid ring vacuum pump.
  - ▶ They are typically used as a vacuum pump but can also be used as a gas compressor.
  - ▶ The function of a liquid ring pump is similar to a rotary vane pump the difference being that the vanes are an integral part of the rotor and churn a rotating ring of liquid to form the compression chamber seal.
  - ▶ Liquid ring pumps are typically powered by an induction motor.
- 

# Image of pump



# Objective

- ▶ Liquid ring vacuum pump encounters severe problems while working on liquid sump. These problems include
  - Leakage in the pump
  - Jamming
  - Reduction in the level of vacuum as time advances
  - cavitations
  - Vibration in the Pump
- ▶ Here the objective of the investigation is to increase the performance and reliability of the pump by modifying its design parameters.

# Literature Review

## A. Shirinov, studied

- ▶ On the Tool™ Booster vacuum pump consists of side channel and Holweck pump Stages. This pump achieves  $10^{-3}$  Pa final pressure and exhausts against Atmosphere. Research is done on side channel pump stages. It shows the ways to Increase the compression and pumping speed while simultaneously reducing size and power consumption. The influences of a backing pump on the power consumption, the form and number of rotor blades on the performance of side channel pump stages have been investigated. It was shown that the power consumption of the pump at final pressure drops from 1150 W to less than 150 W, if a backing pump is used. The properties of double-flow and single-flow side channel stages were compared to each other. It was shown that double-flow stages have a higher pumping speed and a lower compression than single-flow stages.

## Jun Fu Zhao studied

- ▶ A modified pump-out technique, incorporating a novel pump-out hole sealing process, has been developed that enables a high level of vacuum to be achieved between the panes of a vacuum glazing. The modified pump-out method provides several potential opportunities for the fabrication of a vacuum glazing with improved thermal performance.

## Philip C. Eames studied

- ▶ \_Reciprocating and liquid ring vacuum pumps chapter discusses the reciprocating and liquid ring vacuum pump. The best feature of the power pump is its high efficiency. Overall efficiencies normally range from 85% to 94%. The losses of approximately 10% include all those due to belts, gears, bearings, packing, and valves. The direct-acting pump has some of the same advantages as the power pump, plus others. These units are well suited for high-pressure low-flow applications.



# Yueping Fang studied

Rotary displacement pump discusses leak-free rotary displacement pumps. These pumps are employed for transport and circulation duties. Nowadays, these pumps are mainly used in the chemical, petrochemical, cosmetic, foodstuff, paper processing, and bitumen processing industries. The interior of the pump must be lubricated, perhaps once a month, with tallow mixed with a tenth part pulverized graphite. This prevents rust formation in the interior of the pump, and ensures a long service life.

## A. Shirinov, S. Oberbeck

- ▶ The On Tool™ Booster vacuum pump consists of side channel and Holweck pump stages. This pump achieves  $10^{-3}$  Pa final pressure and exhausts against atmosphere. Research is done on side channel pump stages. It shows the ways to increase the compression and pumping speed while simultaneously reducing size and power consumption.



# Zeyu Li, Liansheng Li, Yuanyang Zhao, Gaoxuan Bu, Pengcheng Shu

- ▶ The rarefied gas flows through suction port, scroll clearance and discharge port are treated as leakage of dry scroll vacuum pump (DSVP). The models for predicting the above-mentioned leakage rate were derived in this paper. The model for predicting the heat transfer rate between rarefied gas and working chamber wall was also developed. Then, a general model for describing the working process of DSVP was set up according to the energy and mass conservation principle. This model can be applied to predict the performance of DSVP. The pumping speed for different suction pressures was obtained. Furthermore, the ultimate pressure and power consumption for different speeds were gotten. A good agreement between the theoretical results and experimental data was obtained. Finally, the volume ratio of prototype was changed and its influence on the performance was studied by experiment.

# Project Planning

Finding problem



Selecting the major problems which are affecting the performance of pump



Problem definition of selected problems

Solving the problem



Outcome of investigations



Analysis of outcome results for feasibility



Modification of design according to outcome results



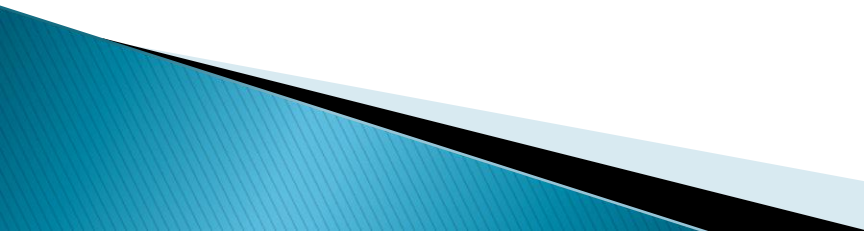
Conclusion

# Work progress:

## Leakage:

When the water is flowing from inlet side there is leakage from the joint where we couple the motor. In order to reduce the cavitations we removed the splitter but it enhances the leakage problem further. Generally company which manufacture vacuum pump uses glance to reduce leakage. But glancing cannot stop leakage problems properly. So we used seal to prevent this problem instead of using glance. Seal shows excellent result to stop the leakage.



- ▶ **Jammed** : Pump jammed because of two reasons the first reason is if the alignment of the shaft is not proper or the vane size is not accurate than the friction will be created between body and vane.
  - ▶ **Cavitations:** when the water flow from the inlet side on that time it creates the bubble in the casing of the pump which creates the cavitations and affects the rotor and eccentricity of the pump. By changing the blade angle and removing the central splitter we can reduce the cavitations problem. By removing the splitter the generated bubble may not be able to burst so we can reduce the cavitations problems to a greater extent.
- 





**Corrosion**

**Improper vacuum:** when the material of eccentricity get wear on that time vacuum will not create properly and it also create the noise because of increasing space between rotor and eccentricity.

**Vibration in the pump:** The reason of this vibration is the shape and the size of vane.





**Eccentricity of the pump:**– Eccentricity helps to create vacuum in the pump. Which break by high pressure of water and because of corrosion.



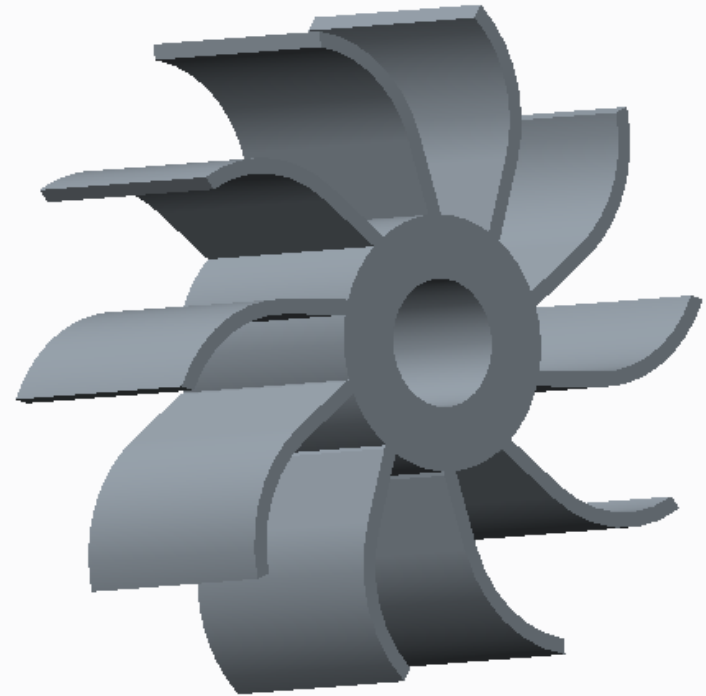
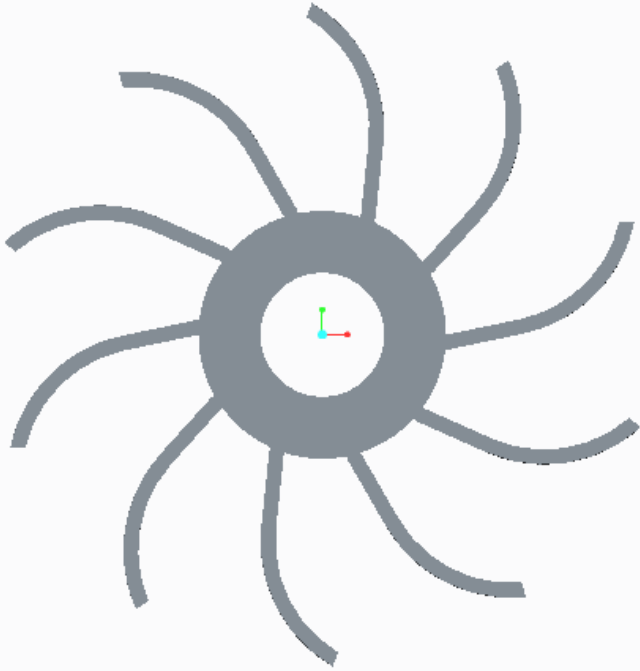


# Different Parts of Vacuum Pump:-

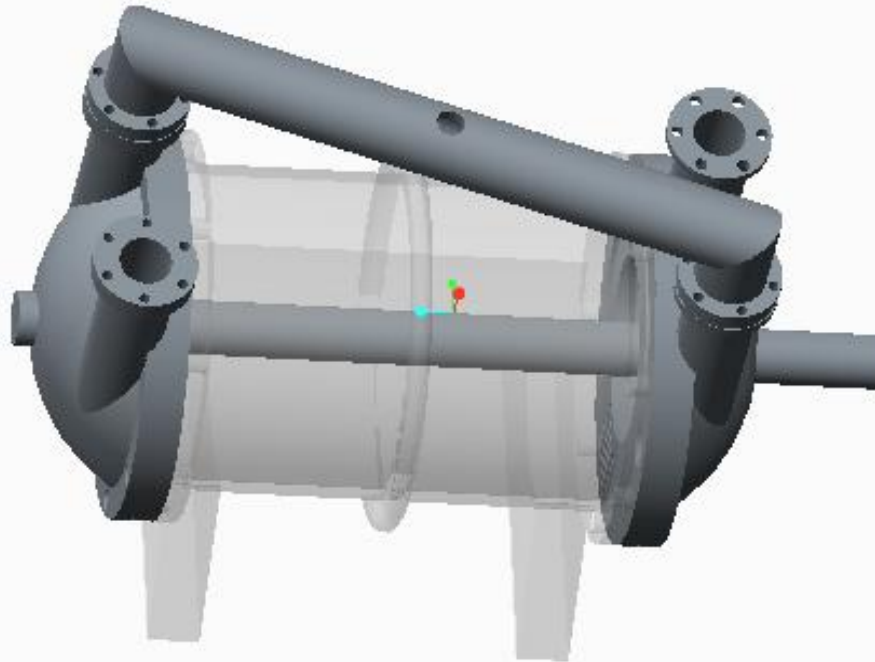
• **MOTOR**: The power source of the pump which drives the shaft. AC motors and DC motors are the most common power sources for pumps, but internal combustion engines (ICEs), hydraulic power, and steam power are other possibilities. Motor is used for generating power for working of the pump. Motor is use to work the vacuum pump which rotates the shaft and which are connected with the shaft of the pump and rotate the impeller so the impeller is run and vacuum create.



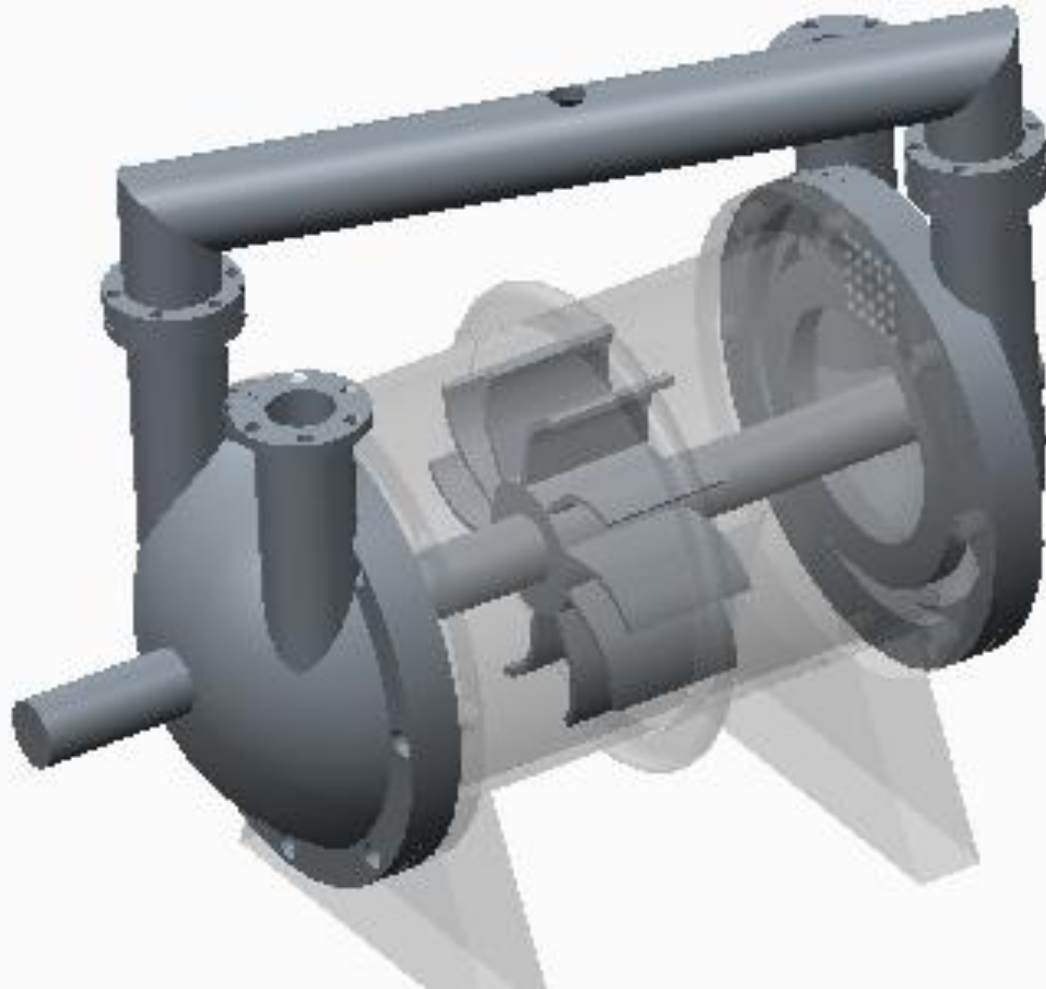
• **IMPELLER**: A rotating disk with a set of vanes coupled to a shaft. When the impeller rotates, it imparts energy to the fluid to induce flow. Flow characteristics of the pump vary widely based on the impeller design.



• **PUMP BODY**: It is covered the all parts of the pump and to provide the safety from dust, material, garbage etc. And helps to create the vacuum by preventing the air from leaking inside.



## Modified Design of Pump



# Calculation:-

1.) Free Air Delivery: -  $\{(K \times T_1) / P_1\} \times \sqrt{H} \times \sqrt{(P_2 / T)} \times 3.6, M^3 /$   
Hr.

2.) Suction Capacity: -  $(F.A.D \times 100) / (100 - \% \text{ of Vacuum}), M^3 /$   
Hr.

Here, K= Nozzle Constant

$T_1$ = Absolute temp. Of free Air

$P_1$ = Pressure of free air

$P_2$ = Absolute pressure after nozzle

H= Pressure drop across nozzle

T= Absolute temp. Of air after nozzle

## 1.) Free Air Delivery:-

$$\begin{aligned} \text{F.A.D} &= \{(K \times T_1) / P_1\} \times \sqrt{H} \times \sqrt{(P_2 / T)} \times 3.6 \\ &= \{(118.41 \times 305.15) / 752\} \times \sqrt{207} \times \sqrt{(736.41 / 298.15)} \times 3.6 \\ &= 3911.81 \text{ M}^3 / \text{Hr.} \end{aligned}$$

## 2.) Suction Capacity:-

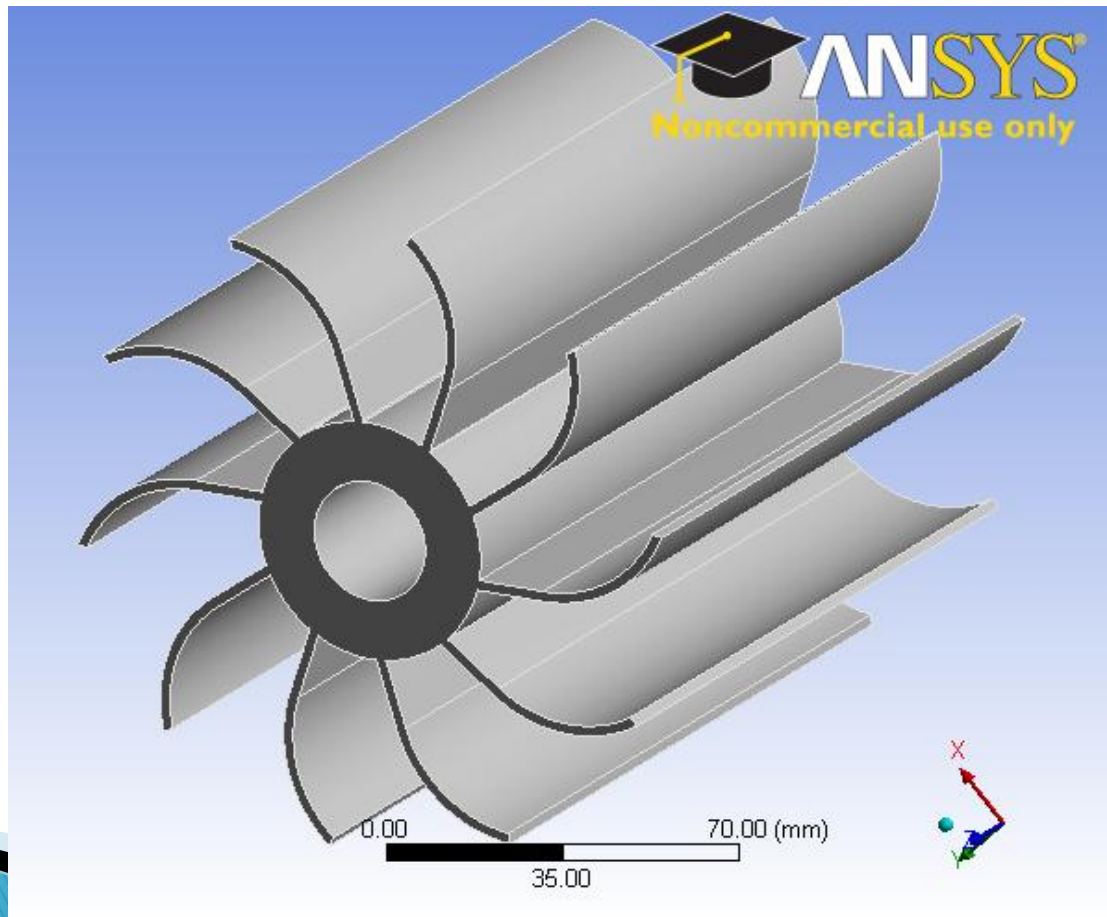
$$\begin{aligned} \text{Suction Capacity} &= (\text{F.A.D} \times 100) / (100 - \% \text{ of Vacuum}) \\ &= (3911.81 \times 100) / (100 - 7.89) \\ &= 4246.79, \text{ M}^3 / \text{Hr.} \end{aligned}$$

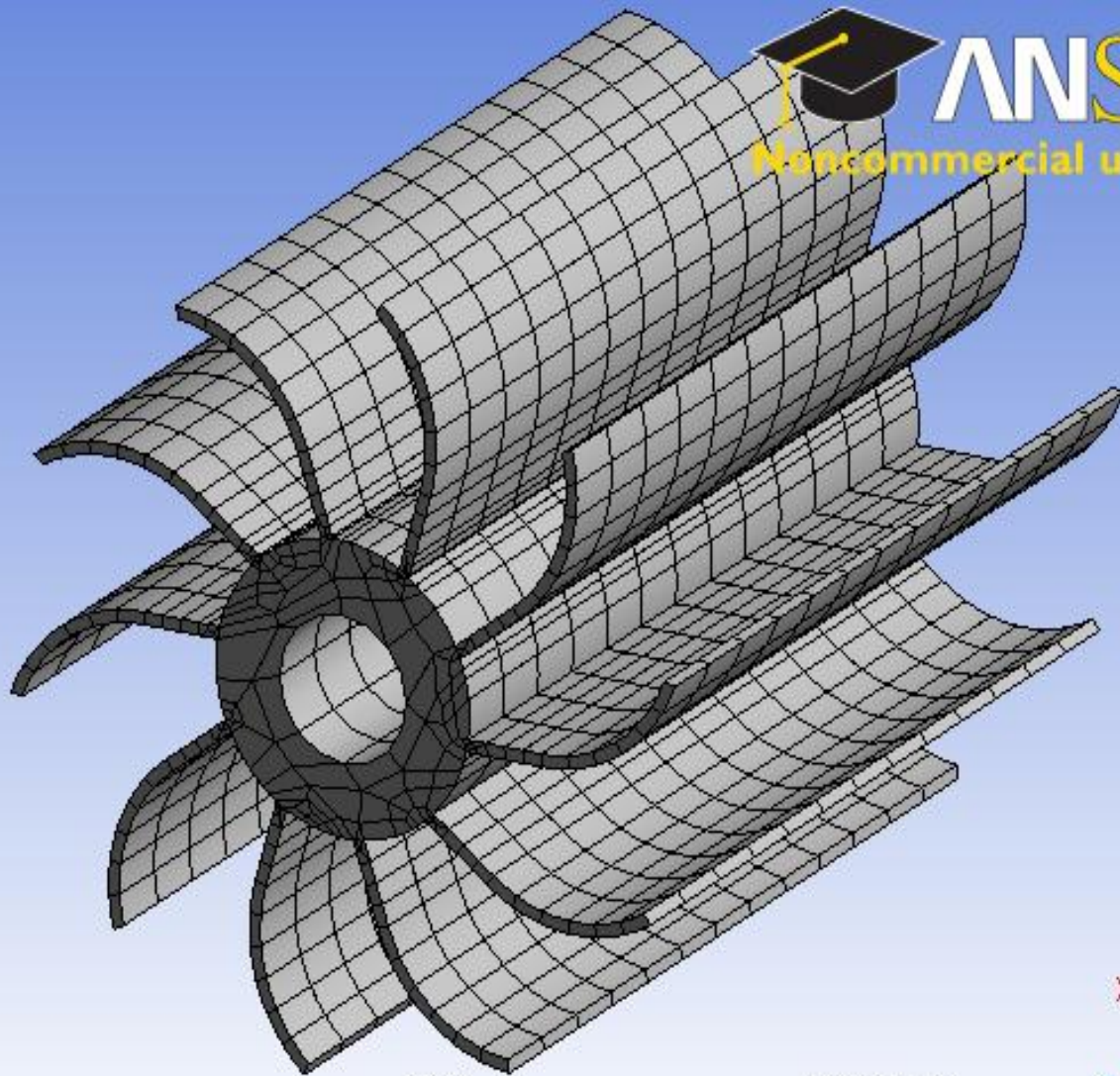
<b>Vacuum in MM of HG</b>	<b>Vacuum %</b>	<b>Current A</b>	<b>Volt V</b>	<b>H MM Wg.</b>	<b>h MM Wg.</b>	<b>F.A.D M<sup>3</sup>/ Hr.</b>	<b>Capacit y M3 / Hr.</b>
<b>60</b>	<b>7.89</b>	<b>120</b>	<b>420</b>	<b>207</b>	<b>212</b>	<b>3911.24</b>	<b>4246.49</b>
<b>100</b>	<b>13.16</b>	<b>138</b>	<b>420</b>	<b>170</b>	<b>175</b>	<b>3551.03</b>	<b>4089.07</b>
<b>200</b>	<b>26.32</b>	<b>160</b>	<b>420</b>	<b>135</b>	<b>138</b>	<b>3170.26</b>	<b>4302.49</b>
<b>500</b>	<b>65.79</b>	<b>272</b>	<b>420</b>	<b>77</b>	<b>80</b>	<b>2401.14</b>	<b>7018.73</b>
<b>700</b>	<b>92.11</b>	<b>262</b>	<b>420</b>	<b>0</b>	<b>0</b>	<b>0.00</b>	<b>0.00</b>



# Analysis:-

## 1. ANALYSIS OF OLD IMPELLER:-





# Static Structural (A5)

<b>Object Name</b>	<i>Static Structural (A5)</i>
<b>State</b>	<b>Solved</b>
<b>Definition</b>	
<b>Physics Type</b>	<b>Structural</b>
<b>Analysis Type</b>	<b>Static Structural</b>
<b>Solver Target</b>	<b>Mechanical APDL</b>
<b>Options</b>	
<b>Environment Temperature</b>	<b>22. °C</b>
<b>Generate Input Only</b>	<b>No</b>

**A: Static Structural**

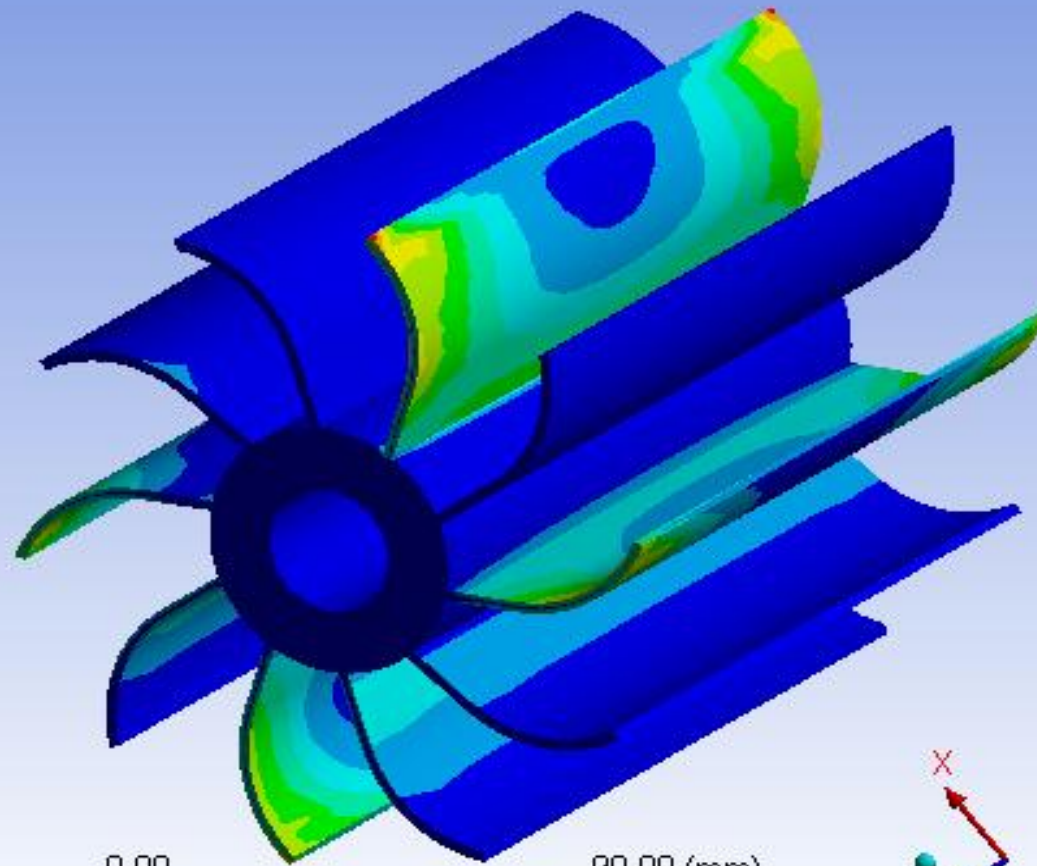
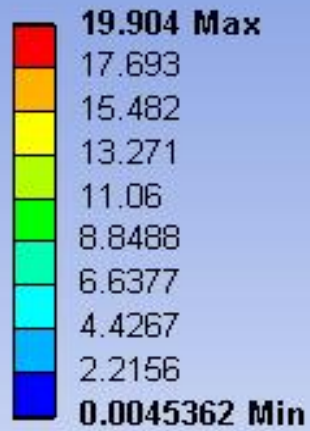
Figure

Type: Equivalent (von-Mises) Stress

Unit: MPa

Time: 1

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**A: Static Structural**

Figure

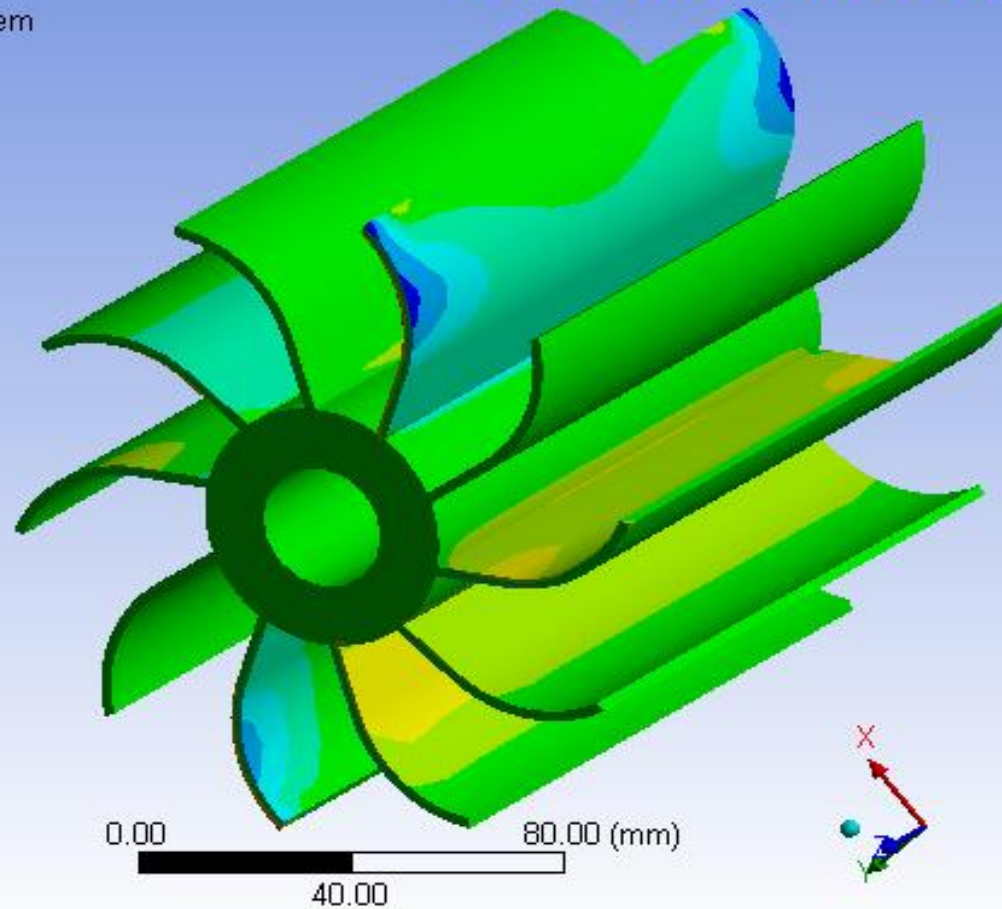
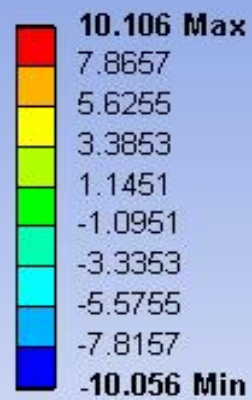
Type: Normal Stress(X Axis)

Unit: MPa

Global Coordinate System

Time: 1

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# A: Static Structural

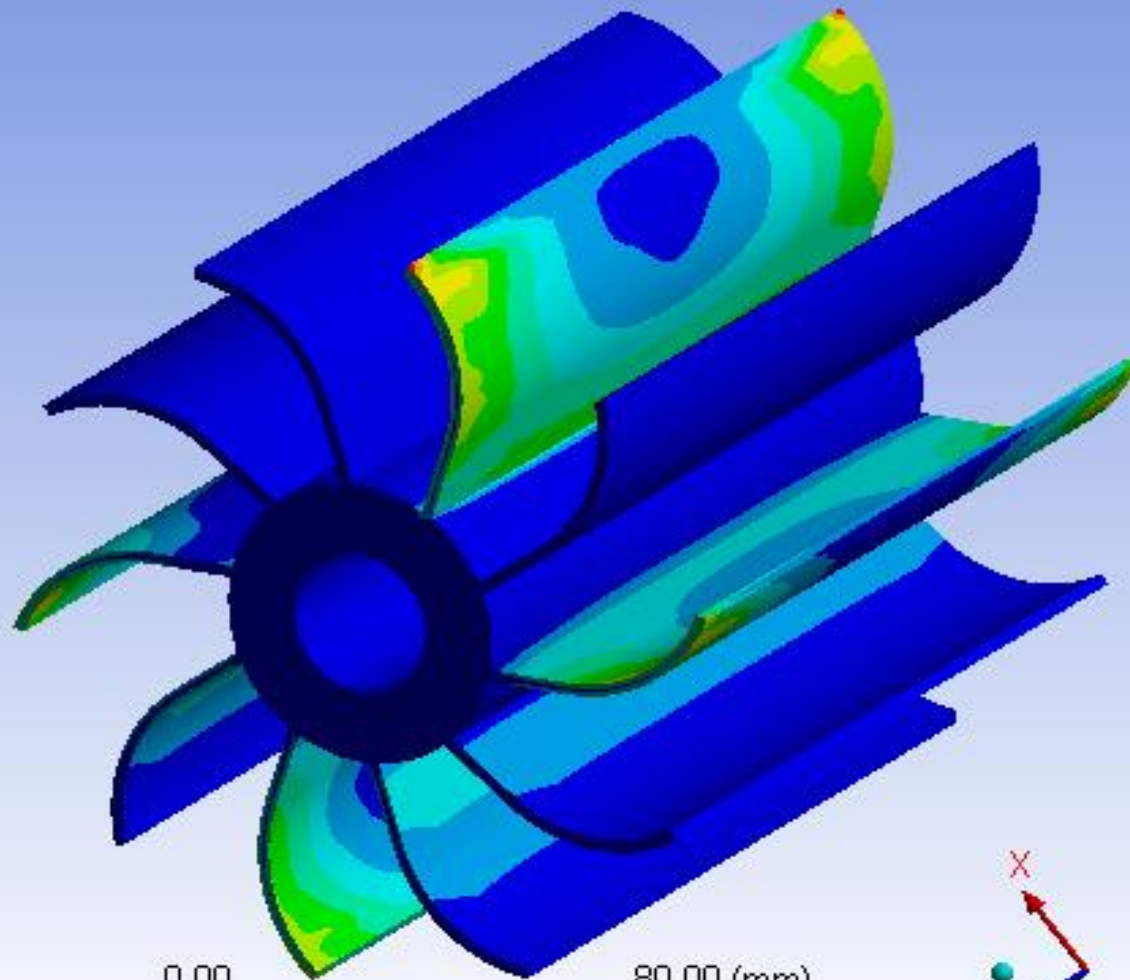
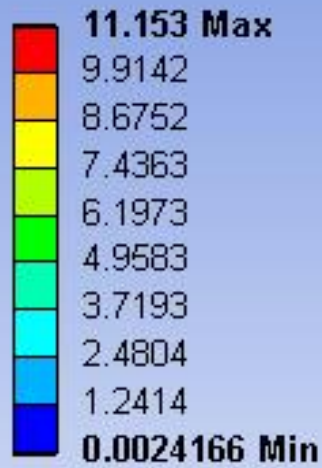
Figure

Type: Maximum Shear Stress

Unit: MPa

Time: 1

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## **Material Data:** *Structural Steel*

**Density**

**7.85e-006 kg mm<sup>-3</sup>**

**Coefficient of Thermal Expansion**

**1.2e-005 C<sup>-1</sup>**

**Specific Heat**

**4.34e+005 mJ kg<sup>-1</sup> C<sup>-1</sup>**

**Thermal Conductivity**

**6.05e-002 W mm<sup>-1</sup> C<sup>-1</sup>**

**Resistivity**

**1.7e-004 ohm mm**



# Alternating Stress Mean Stress

Alternating Stress MPa	Cycles	Mean Stress MPa
3999	10	0
2827	20	0
1896	50	0
1413	100	0
1069	200	0
441	2000	0
262	10000	0
214	20000	0
138	1.e+005	0
114	2.e+005	0
86.2	1.e+006	0

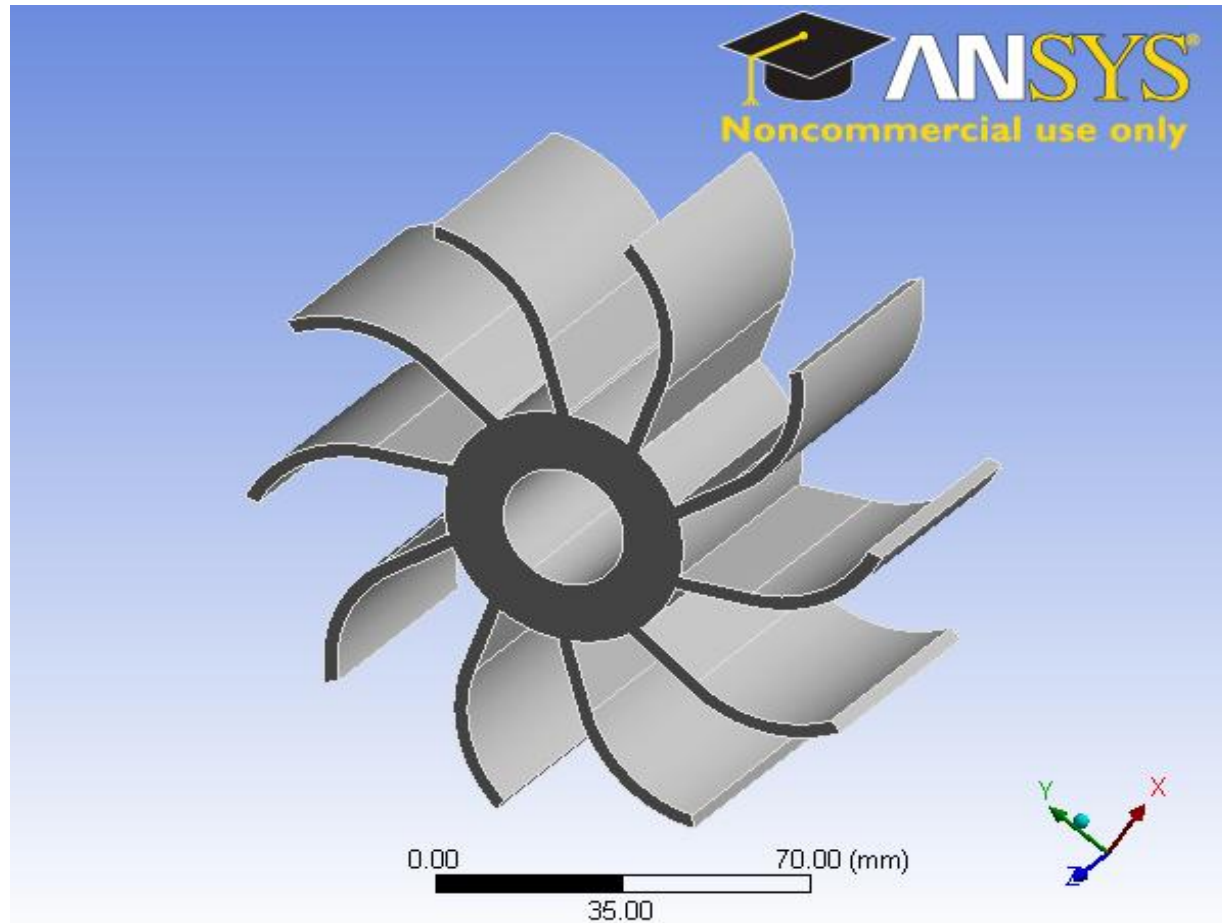
## Strain-Life Parameters

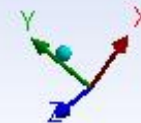
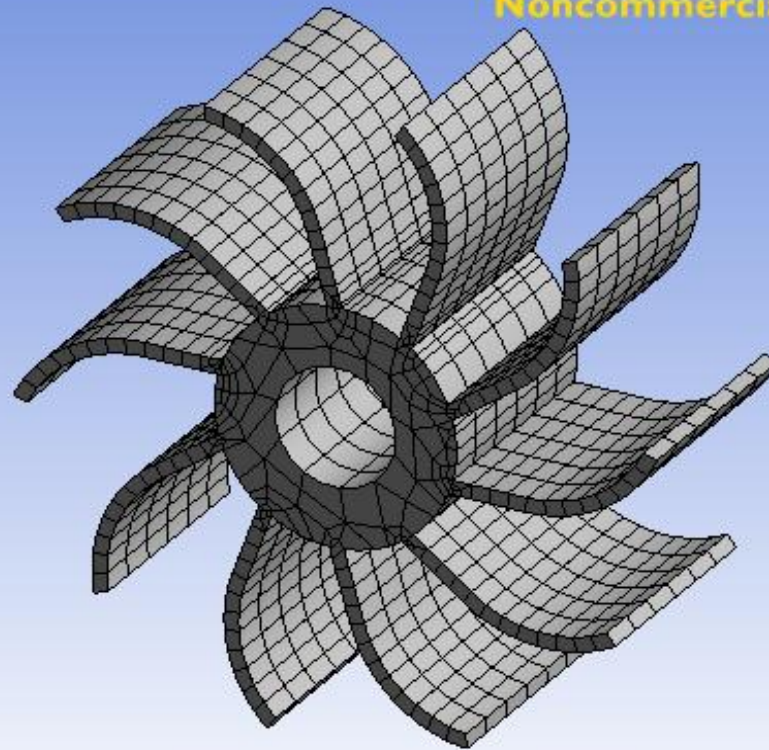
<b>Strength Coefficient MPa</b>	<b>Strength Exponent</b>	<b>Ductility Coefficient</b>	<b>Ductility Exponent</b>	<b>Cyclic Strength Coefficient MPa</b>	<b>Cyclic Strain Hardening Exponent</b>
<b>920</b>	<b>-0.106</b>	<b>0.213</b>	<b>-0.47</b>	<b>1000</b>	<b>0.2</b>

## Isotropic Elasticity

<b>Temperature C</b>	<b>Young's Modulus MPa</b>	<b>Poisson's Ratio</b>	<b>Bulk Modulus MPa</b>	<b>Shear Modulus MPa</b>
	<b>2.e+005</b>	<b>0.3</b>	<b>1.6667e+005</b>	<b>76923</b>

# ANALYSIS OF NEW IMPELLER:-





# Static Structural (A5)

<b>Object Name</b>	<i>Static Structural (A5)</i>
<b>State</b>	<b>Solved</b>
<b>Definition</b>	
<b>Physics Type</b>	<b>Structural</b>
<b>Analysis Type</b>	<b>Static Structural</b>
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<b>Options</b>	
<b>Environment Temperature</b>	<b>22. °C</b>
<b>Generate Input Only</b>	<b>No</b>

# A: Static Structural

Figure

Type: Equivalent (von-Mises) Stress

Unit: MPa

Time: 1

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**A: Static Structural**

Figure

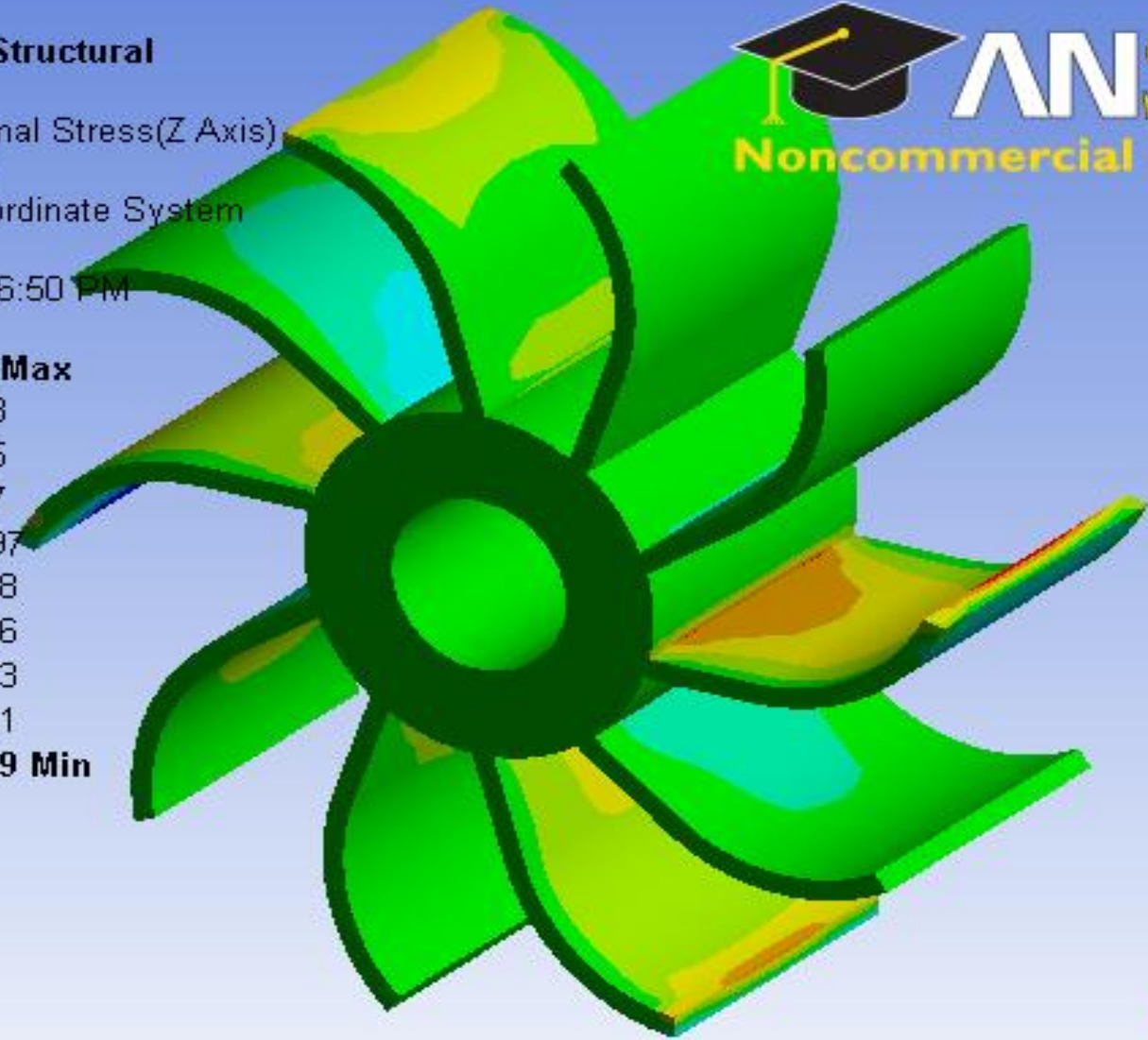
Type: Normal Stress(Z Axis)

Unit: MPa

Global Coordinate System

Time: 1

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**A: Static Structural**

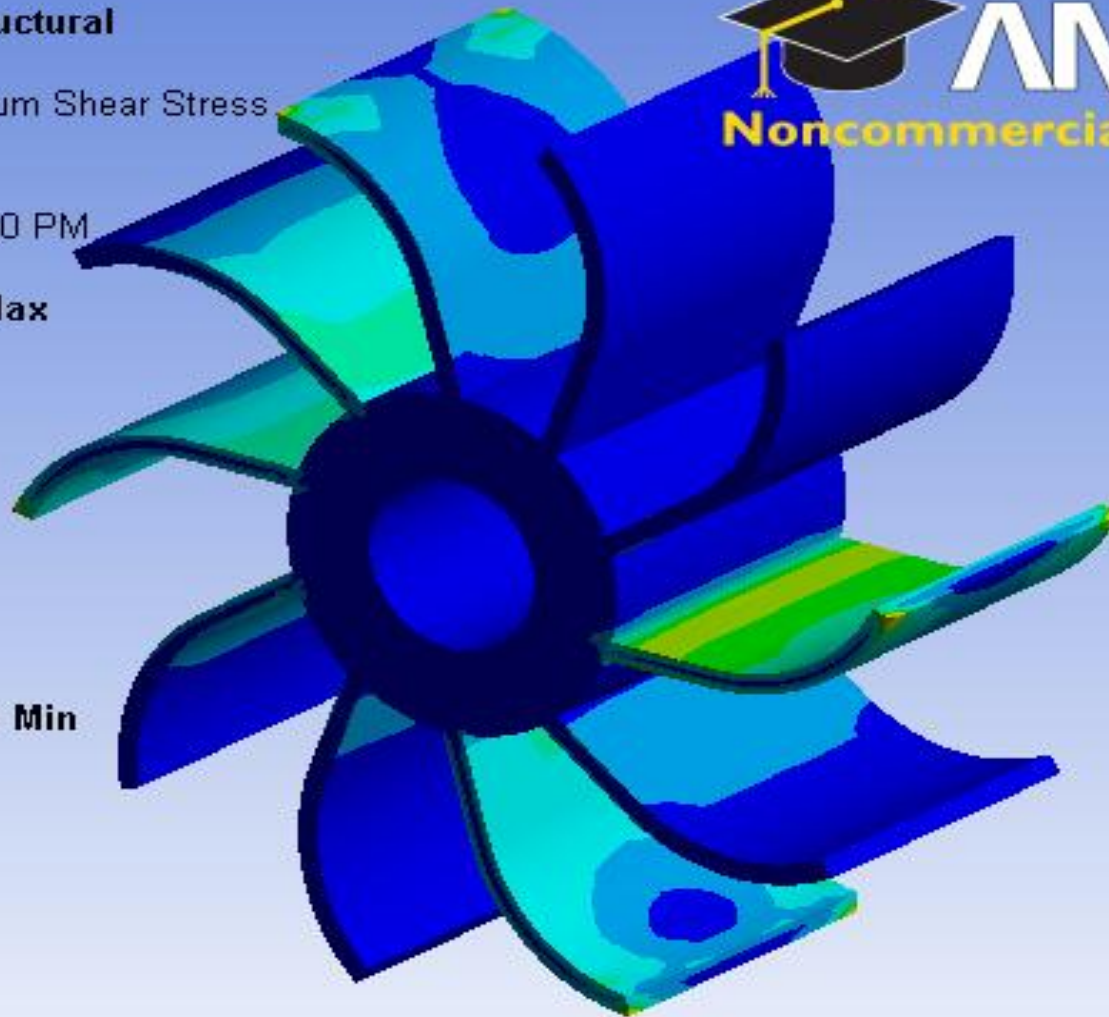
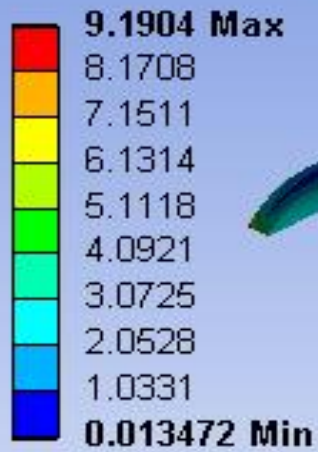
Figure

Type: Maximum Shear Stress

Unit: MPa

Time: 1

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# Material Data

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**Thermal Conductivity**

**6.05e-002 W mm<sup>-1</sup> C<sup>-1</sup>**

**Resistivity**

**1.7e-004 ohm mm**

<b>Alternating Stress MPa</b>	<b>Cycles</b>	<b>Mean Stress MPa</b>
<b>3999</b>	<b>10</b>	<b>0</b>
<b>2827</b>	<b>20</b>	<b>0</b>
<b>1896</b>	<b>50</b>	<b>0</b>
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<b>1069</b>	<b>200</b>	<b>0</b>
<b>441</b>	<b>2000</b>	<b>0</b>
<b>262</b>	<b>10000</b>	<b>0</b>
<b>214</b>	<b>20000</b>	<b>0</b>
<b>138</b>	<b>1.e+005</b>	<b>0</b>
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<b>86.2</b>	<b>1.e+006</b>	<b>0</b>

## Strain-Life Parameters:-

<b>Strength Coefficient MPa</b>	<b>Strength Exponent</b>	<b>Ductility Coefficient</b>	<b>Ductility Exponent</b>	<b>Cyclic Strength Coefficient MPa</b>	<b>Cyclic Strain Hardening Exponent</b>
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## Isotropic Elasticity:-

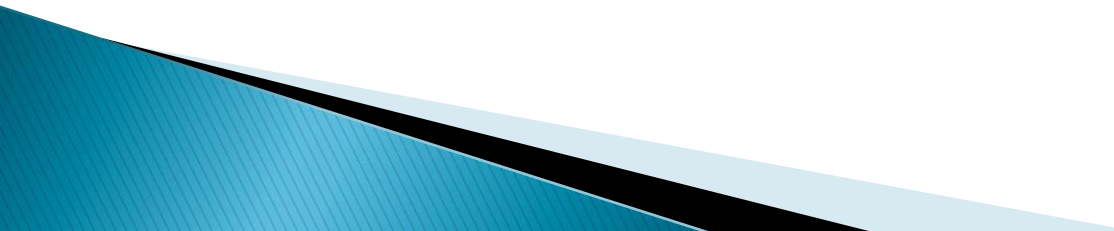
<b>Temperature C</b>	<b>Young's Modulus MPa</b>	<b>Poisson's Ratio</b>	<b>Bulk Modulus MPa</b>	<b>Shear Modulus MPa</b>
	<b>2.e+005</b>	<b>0.3</b>	<b>1.6667e+005</b>	<b>76923</b>

# Conclusion:

- ▶ Form the above project we thoroughly studied various factors which affects pump performance. The factors includes Cavitations, Short term creation of vacuum, Leakage and corrosion in the material. We re-designed the pump parameters to increase the performance. By removing the splitter and re-designing the blades we can increase the performance but removing the splitter leads to higher leakage in the pump. In order to remove this cons we are trying to replace the conventional glance to seal. Further in near future we will change the blade material or apply coating to increase the corrosion resistance of eccentricity material and will use some other technique to remove the vacuum problem.



# References

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